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DIVISION: 06 00 00—WOOD, PLASTICS AND COMPOSITES**Section: 06 02 00—Design Information****REPORT HOLDER:****APA—THE ENGINEERED WOOD ASSOCIATION****EVALUATION SUBJECT:****GLUED-LAMINATED TIMBER COMBINATIONS AND THE GAP COMPUTER PROGRAM****ADDITIONAL LISTEES:****ANTHONY FOREST PRODUCTS CO.****CALVERT COMPANY, INC.****ROSBORO, LLC**

1.0 EVALUATION SCOPE

Compliance with the following codes:

- 2018, 2015, 2012 and 2009 *International Building Code®* (IBC)
- 2018, 2015, 2012 and 2009 *International Residential Code®* (IRC)

Property evaluated:

Structural

2.0 USES

The GAP computer program is utilized to determine design stresses for the specific layups of glued-laminated timbers listed in Tables 1 and 2 of this report.

Glued-laminated timbers manufactured to the glued-laminated timber combinations or single grade layups that have been developed using the GAP program, and that are produced at the facilities listed in Table 3, are recognized as being in compliance with the design parameters indicated in Section 3.0 of this report.

3.0 DESCRIPTION

The GAP computer program is based on the principles of ASTM D3737. It is an alternative method for determining associated allowable design stresses for a given layup combination of glued-laminated timber. The GAP computer program complies with the IBC and the IRC for allowable stress design. The design assumptions discussed in

Sections 3.1 through 3.4 of this report are basic parameters utilized with the development of the allowable design stresses for the combinations listed in Table 1 or single grade layups listed in Table 2. See Section 5.4 for requirements applicable to these parameters.

3.1 Adhesive:

Face and end-joint bonding adhesives comply with ASTM D2559 for exterior or wet use.

3.2 End Joints:

End joints comply with ANSI A190.1 and ASTM D3737.

3.3 Lumber:

Lumber having a nominal thickness of 2 inches or less is glued-laminated into rectangular cross sections complying with industry standards for depth, width, and appearance. Lumber that is E-rated or visually graded complies with rules of applicable approved lumber grading agencies and the procedures set forth in the manufacturer's quality control documentation. Quality control for E-rating and beam fabrication is conducted under the supervision of an approved third-party inspection agency. Grade specifications are included in rules of the applicable approved lumber grading agencies and follow industry classifications and nomenclature as provided in the applicable code.

3.4 Layup:

Beams are fabricated in accordance with ANSI A190.1 using the grade combinations noted in Table 1 or single grade layups noted in Table 2 of this report. Combinations are in accordance with ASTM D3737 requirements. Resawn purlin beams, manufactured by ripping nominally 6-inch beams vertically through their depth into two members of equal width, are permitted to be produced from Canadian spruce-pine (CSP) and spruce-pine-fir (SPF) combinations in this width without any variation in basic grade description or layup procedures.

4.0 DESIGN

The design requirements of structural glued-laminated timber must comply with Section 2306 or 2307 of the IBC, or Sections R502.2 and R802.2 of the IRC, as applicable. Modifications of values for duration of load must comply with the IBC or the IRC, as applicable.

5.0 CONDITIONS OF USE

The specific layups for the glued-laminated timbers described in this report comply with, or are suitable alternatives to what is specified in, those codes listed in

Section 1.0 of this report, subject to the following conditions:

- 5.1** The application of the GAP computer program is limited to the layup combinations shown in Tables 1 or 2. Design stresses for normal conditions of loading must not exceed those set forth in Tables 1 or 2.
- 5.2** Design stresses for combinations noted in Table 1 are for members with four or more laminations stressed primarily in bending due to loads applied perpendicular to the wide faces of the laminations. Design values are included, however, for axial stresses and stresses from bending due to loads applied parallel to the wide faces of the laminations.
- 5.3** Design stresses for combinations noted in Table 2 are for members with two or more laminations stressed primarily axially or in bending due to loads applied parallel to the wide faces of the laminations. Design values are included, however, for stresses from bending due to loads applied perpendicular to the wide faces of the laminations.
- 5.4** The effects of checking of the members are outside the scope of this report.
- 5.5** Glued-laminated timber manufactured to the glued-laminated timber combinations or single grade layups that have been developed using the GAP program, listed in Tables 1 and 2, and that are produced at the facilities listed in Table 3, are recognized as being in compliance with the design parameters indicated in Section 3.0 of this report.

Evaluation of glue-laminated timber manufactured in accordance with this report but produced by manufacturers not listed in Table 3 must be recognized in a current ICC-ES report as being in compliance with the design parameters indicated in Section 3.0 of this report.

- 5.6** The quality program for monitoring the use of the GAP computer program must be in accordance with "Quality Control Requirements for the GAP Computer Program," dated July 26, 2006.

6.0 EVIDENCE SUBMITTED

- 6.1** Program Guide for the GAP Computer Program.
- 6.2** Data in accordance with ASTM D3737.
- 6.3** Quality system documentation.

7.0 IDENTIFICATION

- 7.1** Each glued-laminated beam manufactured using layup combinations determined in accordance with this report and produced at the facilities listed in Table 3 must be identified with the ICC-ES evaluation report number (ESR-1940).

- 7.2** The report holder's contact information is the following:

APA—THE ENGINEERED WOOD ASSOCIATION
7011 SOUTH 19TH STREET
TACOMA, WASHINGTON 98466
(253) 565-6600
www.apawood.org

- 7.3** The additional listees' contact information is the following:

ANTHONY FOREST PRODUCTS CO.
309 NORTH WASHINGTON
EL DORADO, ARKANSAS 71730

CALVERT COMPANY, INC.
218 V STREET
VANCOUVER, WASHINGTON 98661

ROSBORO, LLC
POST OFFICE BOX 20
SPRINGFIELD, OREGON 97477

Table 1 – Reference Design Values for Structural Glued Laminated Softwood Timber Combinations^(a)

Table 1(Continued)– Reference Design Values for Structural Glued Laminated Softwood Timber Combinations^(a) (Members stressed primarily in bending) (Tabulated design values are for normal load duration and dry service conditions.)

Combination Symbol	Bending About X-X Axis				Bending About Y-Y Axis				Axially Loaded				Fasteners Specific Gravity for Fastener Design	
	(Loaded Perpendicular to Wide Faces of Laminations)				(Loaded Parallel to Wide Faces of Laminations ^(b))									
	Extreme Fiber in Bending ^(c)	Compression Perpendicular to Grain	Shear Parallel to Grain	Modulus of Elasticity ^(d)	Extreme Fiber in Bending ^(e)	Compression Perpendicular to Grain	Shear Parallel to Grain	Modulus of Elasticity ^(f)	Tension Parallel to Grain	Compression Parallel to Grain	Shear Parallel to Grain	Modulus of Elasticity ^(g)		
26F-V1	SP/SP	2600	2000	740	300	1.9	0.95	1700	650	260	1.7	1.6	0.85	
26F-V2	SP/SP	2600	2100	740	300	2.0	1.9	1.00	1950	740	260	1.8	0.95	
26F-V3	SP/SP	2600	2100	740	300	2.0	1.9	1.00	1950	650	260	1.9	0.95	
26F-V3M1 ⁽ⁱ⁾	SP/SP	2600	2100	740	300	2.0	1.9	1.00	1950	650	260	1.9	0.95	
26F-V3M2 ^(j)	SP/SP	2600	2100	740	250	2.0	1.9	1.00	1950	650	260	1.9	0.95	
26F-V4	SP/SP	2600	2600	740	300	2.0	1.9	1.00	1700	650	260	1.9	0.95	
26F-V4M1 ^(k)	SP/SP	2600	2600	740	300	2.0	1.9	1.00	1700	650	260	1.9	0.95	
26F-V4M2 ^(l)	SP/SP	2600	2600	740	250	2.0	1.9	1.00	1700	650	260	1.9	0.95	
28F-E1	SP/SP	2800	2300	805	300	2.2 ^(q)	2.1 ^(q)	1.11 ^(q)	1600	650	260	1.8	1.7	
28F-E1M1	SP/SP	2800	2800	805	300	2.2 ^(q)	2.1 ^(q)	1.11 ^(q)	1600	650	260	1.8	1.7	
28F-E2	SP/SP	2800	2800	805	300	2.2 ^(q)	2.1 ^(q)	1.11 ^(q)	2000	650	260	1.8	1.7	
28F-E2M1	SP/SP	2800	2800	805	300	2.2	2.1	1.11	2000	650	260	1.8	1.7	
30F-E1 ^(m)	SP/SP	3000	2400	805	300	2.2 ^(q)	2.1 ^(q)	1.11 ^(q)	1750	650	260	1.8	1.7	
30F-E1M1 ⁽ⁿ⁾	LVL/SP	3000 ^(o)	2400	805	300	2.2	2.1	1.11	1750	650	260	1.8	1.7	
30F-E1M2 ⁽ⁿ⁾	SP/SP	3000 ^(o)	2400	805	300	2.2 ^(q)	2.1 ^(q)	1.11 ^(q)	1750	650	260	1.8	1.7	
30F-E2 ^(m)	SP/SP	3000	3000	805	300	2.2 ^(q)	2.1 ^(q)	1.11 ^(q)	1750	650	260	1.8	1.7	
30F-E2M1 ^(m)	LVL/SP	3000 ^(o)	3000 ^(o)	805	300	2.2	2.1	1.11	1750	650	260	1.8	1.7	
30F-E2M2 ⁽ⁿ⁾	SP/SP	3000 ^(o)	3000 ^(o)	650 ^(p)	300	2.2	2.1	1.11	1750	650	260	1.8	1.7	
30F-E2M3 ⁽ⁿ⁾	LVL/SP	3000 ^(o)	3000 ^(o)	650 ^(p)	300	2.2	2.1	1.11	1750	650	260	1.8	1.7	
Wat-use factors		0.8	0.53	0.875	0.833	0.8	0.53	0.875	0.833	0.8	0.73	See NDS		

For **1 psi = 6.895 Pa**

- (a) The combinations in this table are applicable to members consisting of 4 or more laminations and are intended primarily for members stressed in bending due to loads applied perpendicular to the wide faces of the laminations. However, design values are tabulated for loading both perpendicular and parallel to the wide faces of the laminations. For combinations and design values applicable to members loaded primarily axially or parallel to the wide faces of the laminations, see Table 2. For members of 2 or 3 laminations, see Table 2. The tabulated design values are for dry conditions of use. For wet conditions of use, multiply the tabulated values by the factors shown at the bottom of the table. The tabulated design values are for normal duration of loading. For other durations of loading, see applicable building code.
- (b) The symbols used for species are AC = Alaska cedar, CSP = Canadian spruce-pine, DF = Douglas fir-spruce-pine, SP = Spruce-pine-fir, and SW = Softwood species.
- (c) The tabulated design values in bending, F_{bx} , are based on members 5-18 inches in width by 12 inches in depth by 21 feet in length. For members greater than or equal to 15 inches in depth, F_{bx} must be multiplied by a volume factor, C_v , determined in accordance with applicable building code. The tabulated F_{bx} values require the use of special tension laminations. If these special tension laminations are omitted, the F_{bx} values must be multiplied by 0.75 for members greater than or equal to 15 inches in depth by 21 feet in length. For members less than 15 inches in depth, 20F-E1E1 does not apply.
- (d) The design values for shear, F_{vx} and F_{vy} shall be decreased by multiplying by a factor of 0.72 for non-prismatic members, notched members, and for all members subject to impact or cyclic loading. The reduced design value shall be used for design of members at connections that require special tension laminations.
- (e) Design values are for timber with laminations made from a single piece of lumber across the width or multiple pieces that have been edge bonded. For timber manufactured from multiple piece laminations (across width) that are not edge-bonded, value shall be multiplied by 0.4 for members with 5, 7, or 9 laminations or by 0.5 for all other members. This reduction shall be cumulative with the adjustment in footnote (d).
- (f) See Section 2.5 of ANSI 117 (www.abwabwood.org) for the E_{true} , E_{app} , and E_{min} .
- (g) The values of F_{by} were calculated based on members 12 inches in depth (bending about Y-Y axis). For depths other than 12 inches, the F_{by} values are permitted to be increased by multiplying by the size factor, $(12/d)^{1/9}$, where d is the beam depth in inches. When d is less than 3 inches, use the size adjustment factor for 3 inches.
- (h) The beam depth limitation is as follows - 20F-E1: 15 inches; 24F-V5M2/DF1: 27 inches; 24F-V5M3/DF1 and 24F-VDF1: 24 inches; 26F-E/DF1 and 26F-E/DF1M1: 19-1/2, 11-7/8, 14, 16, and 18 inches in depth.
- (i) 20F-E/DF1 is limited to 1-1/2 to 3-1/2 inches in width and 1-1/2, 9, 9-1/2, 11-7/8, and 14 inches in depth. In this case, wet-use factors must not be applied. Because of the wane, this combination is available only for an industrial appearance characteristic. If wane is omitted, these restrictions must not apply.
- (j) When containing wane, this combination must be used in dry conditions only. In this case, wet-use factors must not be applied. Because of the wane, this combination is available only for an industrial appearance characteristic. If wane is omitted, these restrictions must not apply.
- (k) This combination is limited to 9 to 20 laminations in depth except for 16F-V5M1/SP, which contains a maximum of 1/6 wane on each side and must be 4 laminations or more in depth. For 24F-V/DF1, the F_{by} value is permitted to be increased to 1-3/00 psi for beam depths less than 16 inches. For 24F-V/DF1, the F_{by} value is permitted to be increased to 1-3/00 psi for beam depths of at least 10-1/2 inches. For 26F-E/DF1, the F_{bx} value is permitted to be increased to 2-2/00 psi for beam depths less than 16 inches. For 24F-V/DF1, the F_{bx} value is permitted to be increased to 1-3/00 psi for beam depths less than 16 inches. For 24F-V/DF1, the F_{bx} value is permitted to be increased to 1-3/00 psi for beam depths of at least 10-1/2 inches.
- (l) This combination may be manufactured from either 24F-V4/W/S, 24F-V5M2/W/S, 24F-V5M1/W/S, 24F-E/5M1/W/S, 24F-E/5M1/SP, or 24F-V/3/SP, and is intended primarily for use in header applications.
- (m) This layup combination is limited to nominal 6 inches or less in width. In addition, 30F-E1M1/SP and 30F-E2M1/SP are limited to 1-8 inches or less in depth.
- (n) The beam depth is limited to 16 inches or less for 30F-E2M2/SP and 30 inches or less for 30F-E2M3/SP. The tension lamination requirements for these layups must not be omitted.
- (o) The tabulated design values in bending, F_{bx} , must be multiplied by a volume factor, C_v , determined in accordance with applicable building code using 1/10 as the exponent.
- (p) The allowable compressive stress perpendicular to grain of the beam must be permitted to be increased to the published allowable compressive stress perpendicular to grain of the outermost laminated veneer lumber.
- (q) For 28F and 30F members with more than 15 laminations, $E_{true} = 2.1 \times 10^6$ psi, $E_{app} = 2.0 \times 10^6$ psi, and $E_{min} = 1.06 \times 10^6$ psi.
- (r) This combination may contain lumber with wane. If lumber with wane is used, the design value for shear parallel to grain, F_{bx} , shall be multiplied by 0.67 if wane is allowed on both sides. If wane is limited to one side, F_{bx} shall be multiplied by 0.83. This reduction shall be cumulative with the adjustment in footnote (d).
- (s) This combination may contain wane. If wane lumber is used, F_{vx} must be multiplied by 0.67 if wane is allowed on both sides. If wane is limited to one side, F_{vx} must be multiplied by 0.83. This reduction shall be cumulative with the adjustment in footnote (d).

**Table 2 – Reference Design Values for Structural Glued Laminated Softwood Timber
(Members stressed primarily in axial tension or compression)** (Tabulated design values are for normal load duration and dry service conditions.)

Combination Symbol	Species	Grade	Modulus of Elasticity $0.95 E_{axial}$ (10^6 psi)	E_{axial} (10^6 psi)	All Loading		Axially Loaded		Bending about YY Axis Loaded Parallel to Wide Faces of Laminations		Bending About XX Axis Loaded Perpendicular to Wide Faces of Laminations		Fasteners Specific Gravity for Fastener Design	
							Compression Parallel to Grain		Shear Parallel to Grain ^(a)		Shear Parallel to Grain ^(a)			
							Tension Parallel to Grain	Compression Parallel to Grain	Bending	Bending	Bending	Bending		
Visually Graded Western Species					Compressive Perpendicular to Grain $F_{c\perp}$ (psi)		2 or More Laminations F_t (psi)	4 or More Laminations F_c (psi)	2 or 3 Laminations F_c (psi)	4 or More Laminations F_{by} (psi)	2 Laminations F_{by} (psi)	2 Laminations to 15 in. Deep ^(b) F_{bx} (psi)		
1	DF	L3	1.6	1.5	0.79	560	950	1550	1250	1450	1250	1000	230	1250
2	DF	L2	1.7	1.6	0.85	560	1250	1950	1600	1800	1600	1300	230	1700
3	DF	L2D	2.0	1.9	1.00	650	1450	2300	1900	2100	1850	1550	230	2000
5	DF	L1	2.1	2.0	1.06	650	1650	2400	2100	2400	2100	1800	230	2200
22 ^(e)	SW	L3	1.1	1.0	0.53	315	525	850	725	800	755	725	170	195
70	AC	L2	1.4	1.3	0.69	470	975	1450	1450	1400	1250	1000	230	1350
Visually Graded Southern Pine														
47	SP	N2M12	1.5	1.4	0.74	650	1200	1900	1150	1750	1550	1300	260	1400
48	SP	N2D12	1.8	1.7	0.90	740	1400	2200	1350	2000	1800	1500	260	1600
49	SP	N1M16	1.8	1.7	0.90	650	1350	2100	1450	1950	1750	1500	260	1800
50	SP	N1D14	2.0	1.9	1.00	740	1550	2300	1700	2300	2100	1750	260	2100
Wet-use factors							0.53	0.8	0.73	0.8	0.8	0.8	0.875	0.8
														See NDS

For $S_1 = 1 \text{ psi} = 6.895 \text{ Pa}$

- (a) For members with 2 or 3 laminations, the shear design value for transverse loads parallel to the wide faces of the laminations, F_{vy} , shall be reduced by multiplying by a factor of 0.84 or 0.95, respectively.
- (b) The shear design value for transverse loads applied parallel to the wide faces of the laminations, F_{vy} , shall be multiplied by 0.4 for members with 5, 7, or 9 laminations manufactured from multiple piece laminations (across width) that are not edge bonded. The shear design value, F_{vy} , shall be multiplied by 0.5 for all other members manufactured from multiple piece laminations with unbonded edge joints. This reduction shall be cumulative with the adjustment in footnote (a).
- (c) The design values for shear, F_{vx} and F_{vy} , shall be decreased by multiplying by a factor of 0.72 for non-prismatic members, notched members, and for all members subject to impact or cyclic loading. The reduced design value shall be used for design of members at connections that transfer shear by mechanical fasteners. The reduced design value shall also be used for determination of design values for radial tension and torsion.
- (d) The tabulated F_{bx} values are for members without special tension lams up to 15 inches in depth. If the member depth is greater than 15 inches without special tension lams, the tabulated F_{bx} values must be multiplied by a factor of 0.88. If special tension lams are used, the tabulated F_{bx} values are permitted to be increased by a factor of 1.18 regardless of the member depth.
- (e) When Western Cedars, Western Cedars (North), Western Woods, and Redwood (open grain) are used in combinations for Softwood Species (SW), the design value for modulus of elasticity shall be reduced by 100,000 psi. When Coast Sitka Spruce, Coast Species, Western White Pine, and Eastern White Pine are used in combinations for Softwood Species (SW) tabulated design values for shear parallel to grain, F_{vx} and F_{vy} , shall be reduced by 10 psi, before applying any other adjustments.

Table 3 – Manufacturing Locations

Manufacturer	Location
Anthony Forest Products Co.	256 Cooper Drive, El Dorado, AR 71730
Anthony Forest Products Co.	256 Edison Road, Washington, GA 30676
Calvert Company, Inc.	218 V Street, Vancouver, WA 98661
Calvert Company, Inc.	3559 Truman Road, Washougal, WA 98671
Rosboro	22833 Vaughn Road, Veneta, OR 97487
Rosboro	2509 Main Street, Springfield, OR 97477